

ETA-Danmark A/S Göteborg Plads 1 DK-21590 Nordhavn Tel. +45 72 24 59 00 Fax +45 72 24 59 04 Internet www.etadanmark.dk Authorised and notified according to Article 29 of the Regulation (EU) No 305/2011 of the European Parliament and of the Council of 9 March 2011



# European Technical Assessment ETA-20/0150 of 2023/07/10

I General Part

Technical Assessment Body issuing the ETA and designated according to Article 29 of the Regulation (EU) No 305/2011: ETA-Danmark A/S

Trade name of the construction product:	TCM100 & TCM500 bonded anchor for post- installed rebar connections
Product family to which the above construction product belongs:	Post-installed rebar connections with TCM100 and TCM500 injection mortar
Manufacturer:	Trutek Fasteners Polska Sp z o.o. Al. Krakowska 38 Janki PL-05-090 Raszyn Tel. +48 22 701 93 24 Fax +48 22 100 58 82 Internet <u>www.trutek.com.pl</u>
Manufacturing plant:	Trutek Fasteners Polska Sp z o.o. Factory Plant 1
This European Technical Assessment contains:	19 pages including 14 annexes which form an integral part of the document
This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of:	EAD 330087-01-0601, Systems for post-installed rebar connections with mortar
This version replaces:	The ETA with the same number issued on 2020-02- 07

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## II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

# 1 Technical description of product and intended use

#### Technical description of the product

The subject of this assessment are the post-installed connections, by anchoring or overlap connection joint consisting of steel reinforcing bars (rebars) in existing structures made of normal weight concrete, using injection mortar TCM100 & TCM500 in accordance with the regulations for reinforced concrete construction. The designation TCM100 and TCM500 relates to the cartridge size only. The design of the post-installed rebar connections shall be done in accordance with EN 1992-1-1 (Eurocode 2).

Reinforcing bars with diameters from 8 to 40 mm and TCM100 & TCM500 injection mortar are used for the post-installed rebar connections. The steel element is placed into a drilled hole filled with a mortar and is anchored by the bond between embedded element, injection mortar and concrete.

The characteristic material values, dimensions and tolerances of the anchors not indicated in Annexes shall correspond to the respective values laid down in the technical documentation<sup>1</sup> of this European Technical Assessment.

The product description is given in Annex A.

# 2 Specification of the intended use in accordance with the applicable EAD

The performances given in Section 3 are only valid if the rebar connection is used in compliance with the specifications and conditions given in Annex B

The provisions made in this European Technical Assessment are based on an assumed intended working life of the anchor of 50 years.

The indications given on the working life cannot be interpreted as a guarantee given by the producer or Assessment Body, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

<sup>1</sup> The technical documentation of this European Technical Assessment is deposited at ETA-Danmark and, as far as relevant for the tasks of the Notified bodies involved in the attestation of conformity procedure, is handed over to the notified bodies.

# **3** Performance of the product and references to the methods used for its assessment

#### 3.1 Characteristics of product

#### Mechanical resistance and stability (BWR1):

The essential characteristics are detailed in the Annex C.

#### Safety in case of fire (BWR2):

Reaction to fire: Rebar connections satisfy requirements for Class A1.

Resistance to fire: See annex C

#### Hygiene, health and the environment (BWR3):

No performance assessed.

#### Safety in use (BWR4):

For basic requirement Safety in use the same criteria are valid for Basic Requirement Mechanical resistance and stability (BWR1).

Other Basic Requirements are not relevant.

#### 3.2 Methods of assessment

The assessment of fitness of the anchor for the intended use in relation to the requirements for mechanical resistance and stability and safety in use in the sense of the Basic Requirements 1 and 4 has been made in accordance with the EAD 330087-01-0601, Systems for post-installed rebar connections with mortar.

# 4 Assessment and verification of constancy of performance (AVCP)

#### 4.1 AVCP system

According to the decision 96/582/EC of the European Commission, the system(s) of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) is 1.

# 5 Technical details necessary for the implementation of the AVCP system, as foreseen in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited at ETA-Danmark prior to CE marking

Issued in Copenhagen on 2023-07-10 by

Thomas Bruun Managing Director, ETA-Danmark

# Installation post installed rebar

Figure A1: Overlapping joint for rebar connections of slabs and beams

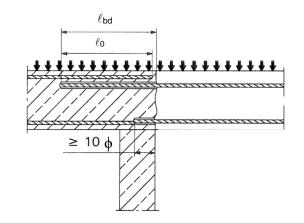


Figure A3: End anchoring of slabs or beams (e.g. designed as simply supported)

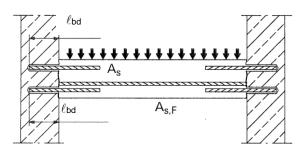


Figure A2: Overlapping joint at a foundation of a wall or column where the rebars are stressed in tension

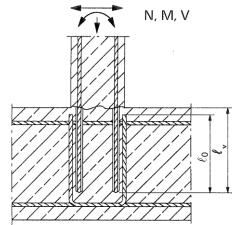
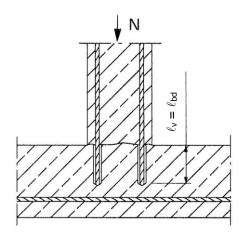
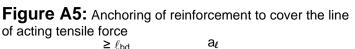
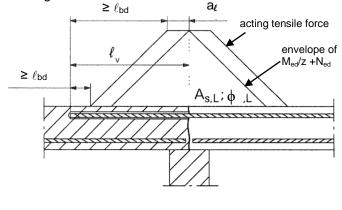


Figure A4: Rebar connection for components stressed primarily in compression. The rebars sre stressed in compression







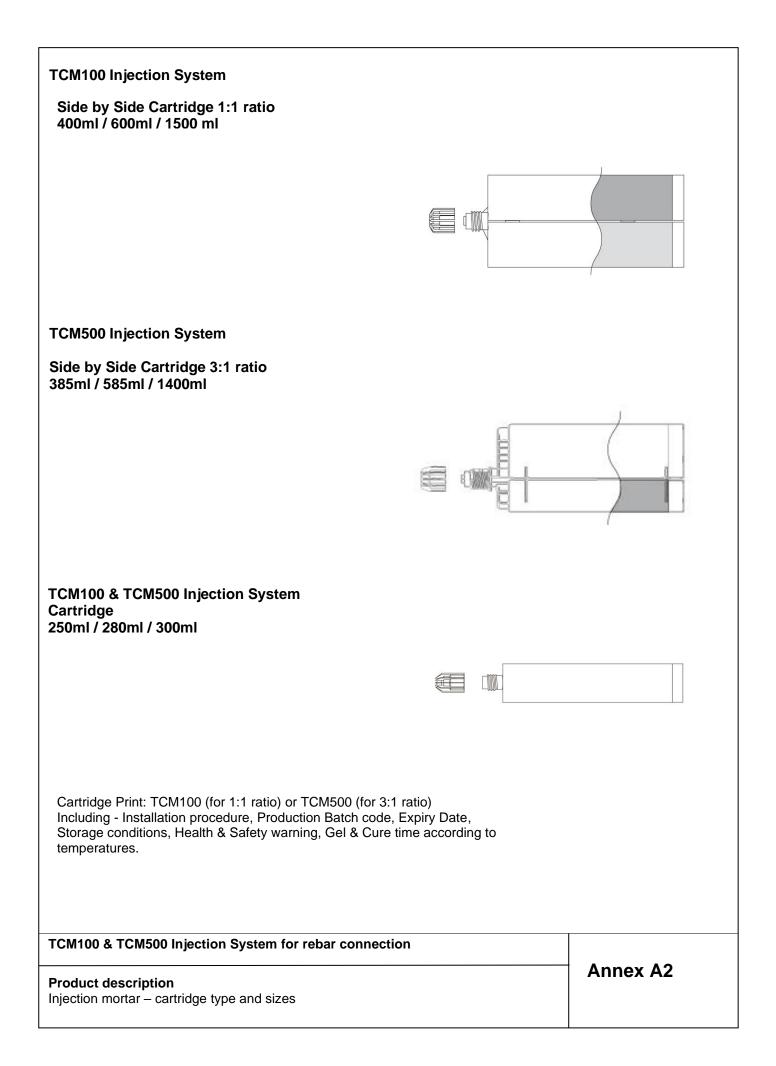
#### Note to Figure A1 to A5:

In the Figures no transverse reinforcement is plotted, the transverse reinforcement shall comply with EN 1992-1-1:2004+AC:2010.

Preparing of joints according to Annex B 2

TCM100 & TCM500 Injection System for rebar connection **Product description** Installed condition and examples of use for rebars

Annex A1



## Page 8 of 19 of European Technical Assessment no. ETA-20/0150, issued on 2023-07-10

Mixer	T-Flow Mixer™
Epoxy Mixer	
Mixer Extension	
Mixer Extension Short	
Vixer Extension Long	
Minimum value of related rip area Rib height of the bar shall be in th (\$ Nominal diameter of the bar; h	
Minimum value of related rip area Rib height of the bar shall be in th (¢: Nominal diameter of the bar; I Table A1: Materials	a f <sub>R,min</sub> according to EN 1992-1-1:2004+AC:2010 the range 0,05 $\phi \le h \le 0,1\phi$
Minimum value of related rip area Rib height of the bar shall be in the (\$ Nominal diameter of the bar; h	a f <sub>R,min</sub> according to EN 1992-1-1:2004+AC:2010 the range $0,05\phi \le h \le 0,1\phi$ h: Rip height of the bar) Material Bars and de-coiled rods class B or C
Minimum value of related rip area Rib height of the bar shall be in th (\$\phi: Nominal diameter of the bar; f Table A1: Materials Designation	a f <sub>R,min</sub> according to EN 1992-1-1:2004+AC:2010 the range $0,05\phi \le h \le 0,1\phi$ h: Rip height of the bar) $\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$

## Specifications of intended use

#### Anchorages subject to:

- Static and quasi-static loads.
- Seismic loading
- Fire exposure

#### **Base materials:**

- Reinforced or unreinforced normal weight concrete according to EN 206:2013+A1:2016.
- Strength classes C12/15 to C50/60 according to EN 206:2013+A1:2016.
- Maximum chloride concrete of 0,40% (CL 0.40) related to the cement content according to EN EN 206:2013+A1:2016.
- Non-carbonated concrete.

Note: In case of a carbonated surface of the existing concrete structure the carbonated layer shall be removed in the area of the post-installed rebar connection with a diameter of  $\phi$  + 60 mm prior to the installation of the new rebar.

The depth of concrete to be removed shall correspond to at least the minimum concrete cover in accordance with EN 1992-1-1:2004+AC:2010.

The foregoing may be neglected if building components are new and not carbonated and if building components are in dry conditions.

#### **Temperature Range:**

• - 40°C to +80°C (max. short term temperature +80°C and max long term temperature +50°C).

#### Design:

- Anchorages are designed under the responsibility of an engineer experienced in anchorages and concrete work.
- Verifiable calculation notes and drawings are prepared taking account of the forces to be transmitted.
- Design according to EN 1992-1-1:2004+AC: 2010 for static loading and EN 1998-1 for seismic loading. The actual position of the reinforcement in the existing structure shall be determined on the basis of the construction documentation and taken into account when designing.
- Anchorages under fire exposure are designed in accordance with EN 1992 1- 2:2004+AC:2008

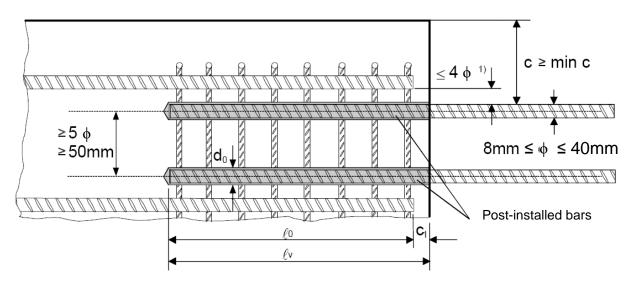
#### Installation:

- · Dry or wet concrete.
- It must not be installed in flooded holes.
- Hole drilling by hammer drill (HD) or compressed air drill mode (CD).
- The installation of post-installed rebar resp. tension anchors shall be done only by suitable trained installer and under supervision on site; the conditions under which an installer may be considered as suitable trained and the conditions for supervision on site are up to the Member States in which the installation is done.
- Check the position of the existing rebars (if the position of existing rebars is not known, it shall be determined using a rebar detector suitable for this purpose as well as on the basis of the construction documentation and then marked on the building component for the overlap joint).

TCM100 & TCM500 Injection System for rebar connection	Annex B1
Intended use	
Specifications	

## Figure B1: General construction rules for post-installed rebars

- Only tension forces in the axis of the rebar may be transmitted.
- The transfer of shear forces between new concrete and existing structure shall be designed additionally according to EN 1992-1-1:2004+AC: 2010.
- The joints for concreting must be roughened to at least such an extent that aggregate protrude.



<sup>1)</sup> If the clear distance between lapped bars exceeds 4φ, then the lap length shall be increased by the difference between the clear bar distance and 4φ.

The following applies to Figure B1:

- c concrete cover of post-installed rebar
- c1 concrete cover at end-face of existing rebar
- min c minimum concrete cover according to Table B1 and to EN 1992-1-1:2004+AC:2010, Section 4.4.1.2
   φ diameter of post-installed rebar
- lap length, according to EN 1992-1-1:2004+AC: 2010, Section 8.7.3 for static loading and according to EN 1998-1, chapter 5.6.3 for seismic loading
- $\ell_v$  effective embedment depth,  $\geq \ell_0 + c_1$
- d<sub>0</sub> nominal drill bit diameter, see Annex B5

TCM100 & TCM500 Injection System for rebar connection	Annex B2
Intended use General construction rules for post-installed rebars	Annex D2

# Table B1: Minimum concrete cover cmin<sup>1)</sup> ofpost-installed rebar depending of drilling method

Drilling aid

Drilling method	Rebar diameter	Without drilling aid	With drilling aid
Hommor drilling (HD)	< 25 mm	$30 \text{ mm} + 0,06 \cdot \ell_{v} \ge 2 \phi$	$30 \text{ mm} + 0,02 \cdot \ell_{v} \ge 2 \phi$
Hammer drilling (HD)	≥ 25 mm	$40 \text{ mm} + 0,06 \cdot \ell_{v} \ge 2 \phi$	$40 \text{ mm} + 0,02 \cdot \ell_{v} \ge 2 \phi$
Comprosed oir drilling (CD)	< 25 mm	50 mm + 0,08 · ℓ <sub>v</sub>	50 mm + 0,02 $\cdot \ell_v$
Compressed air drilling (CD)	≥ 25 mm	60 mm + 0,08 · $\ell_v$	60 mm + 0,02 · $\ell_v$

see Annex B2 & Figures B1

1)

Comments: The minimum concrete cover acc. EN 1992-1-1:2004+AC:2010 must be observed

 Table B2:
 Minimum concrete cover cmin, seis
 for seismic loading:

Design conditions	Distance of 1st edge	Distance of 2nd edge
Edge	≥ 4 ¢	≥ 8 <b>φ</b>
Corner	≥ 6 ¢	≥ 6 <b>φ</b>

#### Table B3: maximum embedment depth $\ell_{v,max}$

Rebar	l [mm]	
φ	$\ell_{ m v,max}$ [mm]	
8 mm to 40 mm	750	

## Table B4: Base material temperature, gelling time and curing time

Concrete temperature	Gelling working time <sup>1)</sup>	Minimum curing time in dry concrete	Minimum curing time in wet concrete
+ 5 °C	70 min <sup>2)</sup>	48 h	96 h
+ 10 °C	32 min <sup>2)</sup>	40 h	80 h
+ 15 °C	28 min <sup>2)</sup>	30 h	60 h
+ 20 °C	25 min <sup>2)</sup>	18 h	36 h
+ 25 °C	22 min <sup>2)</sup>	17 h	34 h
+ 30 °C	20 min <sup>2)</sup>	16 h	32 h
+ 40 °C	18 min <sup>2)</sup>	12 h	24 h

 $^{1)}\,t_{gel}$ : maximum time from starting of mortar injection to completing of rebar setting.

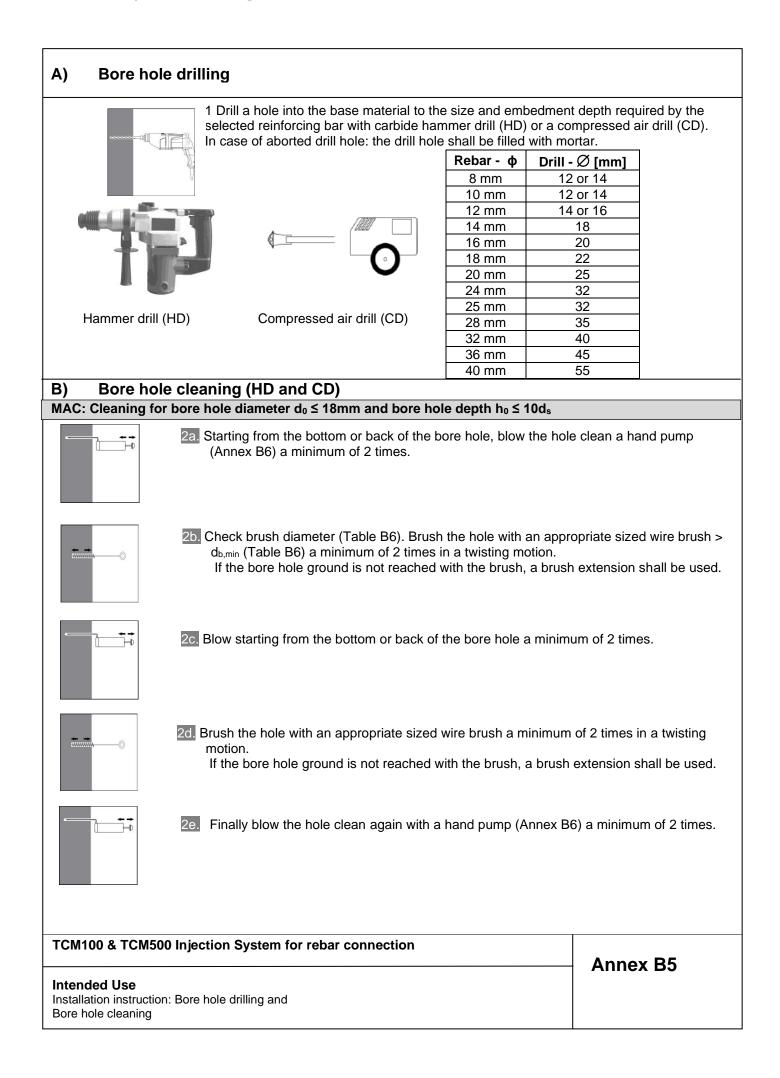
<sup>2)</sup> Cartridge temperature <u>must</u> be at minimum +15°C

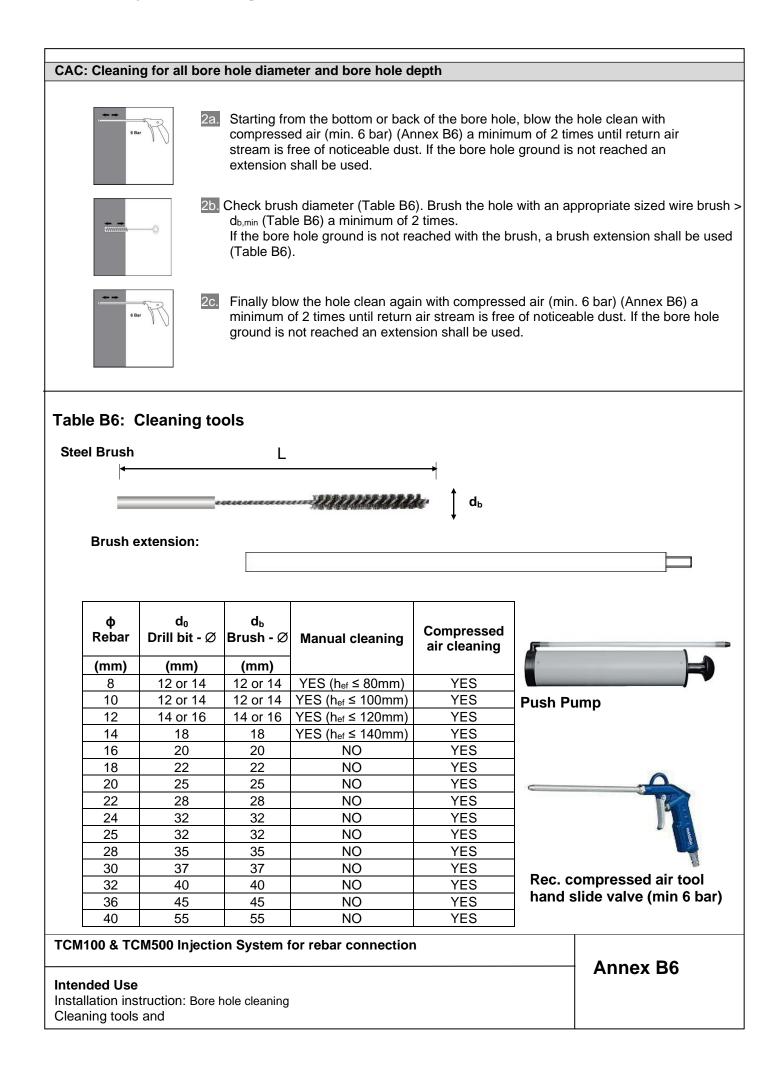
TCM100 & TCM500 Injection System for rebar connection	Annov D2
Intended use Minimum concrete cover Maximum embedment depth / working time and curing times	Annex B3

# Table B5: Dispensing tools

Resin injection pump details	Size Contriduce	Turne
mage	Size Cartridge	Туре
	400 ml 1:1 600 ml 1:1 385 / 585 ml 3:1	Manual
	250 / 280 / 300 ml	Manual
	400 ml 1:1 600 ml 1:1 385 / 585 ml 3:1	Battery
	7.4v Tool	
	400 ml 1:1 600 ml 1:1 385 / 585 ml 3:1 250 / 280 / 300 ml	Pneumatic
	1400 ml 3:1 1500 ml 1:1	Pneumatic

TCM100 & TCM500 Injection System for rebar connection	Annex B4
Intended Use Dispensing tools	





C)

Preparation of bar and cartridge

	+ +	1 tł F	he correct dispensin or every working int	tatic-mixing nozzle to g tool. erruption longer than for every new cartrid	the recommended	working time
	h <sub>ef</sub>	4.		e reinforcing bar into		
	-		•	· •		einforcing bar and insert
	terre t <sub>gel</sub>			o verify hole and dept should be free of dirt		r foreign material.
	×	<u>ج</u>		grey colour, but a min		tely the mortar until it trokes, and discard non-
D) Fil	lling the	6.	Starting from the bot approximately two-th the hole fills to avoid	ttom or back of the cle hirds with adhesive. S I creating air pockets. orking times given in T	Slowly withdraw the	fill the hole up to static mixing nozzle as
Table B7	7: Maxim	num anc	horage depth a	nd mixer extensi		
	Dr		Hand or k		e:All sizes	natio tool
Bar size	bit	-Ø	-	oattery tool	Pneur	natic tool
ф	bit - H	- Ø D	lv,max	Dattery tool Mixer extension	Pneur I <sub>v,max</sub>	Mixer extension
	bit - Hi [mi	- Ø D m]	l <sub>v,max</sub> [mm]	Dattery tool Mixer extension Short/Long	Pneur I <sub>v,max</sub> [mm]	Mixer extension Short/Long
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 TCM100 & TCM500 Injection System for rebar connection
 Annex B7

 Intended Use
 Installation instruction: Preparation of bar and cartridge

 Filling the bore hole
 Filling the bore hole

	Mi	xer Extension Short					
	Mixer Ex	tension Short + Long					
	III [						
E) Inserting the reba	ır						
t <sub>sel</sub>	Push the reinforcing bar into the anchor hole while turnin positive distribution of the adhesive until the embedment The bar should be free of dirt, grease, oil or other foreign	depth is reached.					
8.	_						
t <sub>cure</sub>	Observe gelling time $t_{gel}$ . Attend that the gelling time can material temperature (see Table B3). It is not allowed to r time $t_{gel}$ has elapsed. Allow the adhesive to cure to the specified time prior to a move or load the bar until it is fully cured (attend Table B3) $t_{cure}$ has elapsed, the add-on part can be installed.	nove the bar after gelling pplying any load. Do not					
Intended Use	System for rebar connection	Annex B8					
Installation instruction: Filling t Inserting rebar	he bore hole						

# Essential characteristic under static loading:

Minimum anchorage length and minimum lap length

The minimum anchorage length  $\ell_{b,min}$  and the minimum lap length  $\ell_{0,min}$  according to EN 1992-1-1:2004+AC:2010 ( $\ell_{b,min}$  acc. to Eq. 8.6 and Eq. 8.7 and  $\ell_{0,min}$  acc. to Eq. 8.11) shall be multiply by the amplification factor  $\alpha_{lb}$  according to Table C1.

The design bond strength  $f_{bd}$  according to EN 1992-1-1:2004+AC:2010 (Eq.8.3) shall be multiplied by the factor  $k_b$  according to Table C2 to determine the design values of the ultimate bond stress for post installed rebars  $f_{bd,PIR}$ , which are given in Table C3.

Concrete class	Drilling method	Rebar size	Amplification factor $\alpha_{lb}$	
C12/15 to C45/55	Hammer drilling (HD) and compressed air drilling (CD)	8 mm to 25 mm	1,0	
C50/60	Hammer drilling (HD) and compressed air drilling (CD)	8 mm to 25 mm	1,1	
C12/15 to C50/60	Hammer drilling (HD) and compressed air drilling (CD)	28 mm to 40 mm	1.0	

## Table C2: Bond efficiency factor kb

Bohor Ø		Bond efficiency factor k <sub>b</sub> [-] Concrete class							
Rebar - Ø									
Diameter	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
8 to 25 mm						1.0	1,0	1,0	1,0
28 to 36 mm	1,0	1,0	1,0	1,0	1,0	1,0	1,0	0,93	0,93
40 mm						0,88	0,81	0,85	0,79

# Table C3: Design values of the ultimate bond stress $f_{bd, PIR}$ in N/mm<sup>2</sup> for all drilling methods for good conditions

according to EN 1992-1-1:2004+AC:2010 for good bond conditions (for all other bond conditions multiply the values by 0.7). For rebar diameter sizes > 32mm,  $f_{bd}$  shall be multiplied with  $\eta_2$  according to EN 1991-1-1, section 8.4.2. See also the important notes reported at the end of Annex C2 for additional information.

Rebar - Ø	Bond resistance fbd, PiR [N/mm <sup>2</sup> ]								
Repai - Ø		Concrete class							
Diameter	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
8 to 25 mm						3,4	27	4,0	4,3
28 to 36 mm	1,6	2,0	2,3	2,7	3,0	5,4	3,7	3,7	4,0
40 mm						3,0	3,0	3,4	3,4

mplification factor $\alpha_{lb}$	Annex C1
Performances for static loading	
Design values of ultimate bond resistance fbd,PIR	
	1

## Essential characteristic under seismic loading:

Minimum anchorage length and minimum lap length

The minimum anchorage length  $\ell_{b,min}$  and the minimum lap length  $\ell_{0,min}$  according to

EN 1992-1-1:2004+AC:2010 ( $\ell_{b,min}$  acc. to Eq. 8.6 and Eq. 8.7 and  $\ell_{0,min}$  acc. to Eq. 8.11) shall be multiply by the amplification factor  $\alpha_{lb}$  according to Table C1.

The design bond resistance  $f_{bd,seis}$  it is given in the table C6. It is obtained by multiplying the design bond resistance  $f_{bd}$  according to EN1992-1-1 (Eq. 8.3) by the bond efficiency factor  $k_{b,seis}$  according to Table 4.

## Table C4: Bond efficiency factor under seismic loading k<sub>b,seis</sub>

Deher Ø	Bond efficiency factor under seismic loading k <sub>b,seis</sub> [-]								
Rebar - Ø	Concrete class								
Diameter	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60	
8 to 20 mm					1	1			
24 mm			1	1	1	1	0,92	0,86	
25 mm					'		0,84	0,79	
28 mm	1	1				0,91	0,84	0,71	
30 mm	I				0.00	0,90 0	0,82	0,76	0,71
32 mm					0,90	0,73	0,67	0,63	
36 mm			0,86	0,76	0,68	0,63	0,58	0,54	
40 mm		0,86	0,74	0,66	0,59	0,54	0,50	0,47	

# Table C5: Design values of the ultimate bond stress f<sub>bd, seism</sub> in N/mm<sup>2</sup> for all drilling methods for good conditions under seismic loading

according to EN 1992-1-1:2004+AC:2010 for good bond conditions (for all other bond conditions multiply the values by 0.7)

Rebar - Ø	Bond resistance under seismic loading f <sub>bd, seis</sub> [N/mm²] Concrete class							
Repai - Ø								
Diameter	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
8 to 20 mm							4,0	4,3
24 mm		2,3 2,7 3,0 3,4		3,7	3,7	3,7		
25 mm			2,7	3,0	3,4		3,4	3,4
28 mm	2.0					3,4	3,4	3,0
30 mm	2,0				2.0	3,0	3,0	3,0
32 mm					3,0	2,7	2,7	2,7
36 mm	1		2,3	2,3	2,3	2,3	2,3	2,3
40 mm		2,0	2,0	2,0	2,0	2,0	2,0	2,0

#### Important notes for static and seismic loading:

- If Nationally Determined Parameter for  $\alpha_{ct}$  differs from the recommended value given in EN 1991-1-1,  $f_{bd}$  shall be multiplied with  $\alpha_{ct}$
- If Nationally Determined Parameter for  $\gamma_c$  differs from the recommended value given in EN 1991-1-1,  $f_{bd}$  shall be multiplied with 1,5 /  $\gamma_c$
- For all other than good bond conditions  $f_{bd}$  shall be multiplied with  $\eta_1$  according to EN 1991-1-1, section 8.4.2
- For rebar diameter sizes > 32mm,  $f_{bd}$  shall be multiplied with  $\eta_2$  according to EN 1991-1-1, section 8.4.2

#### TCM100 & TCM500 Injection System for rebar connection

## Performances for seismic loading

Design values of ultimate bond resistance  $f_{bd,seis}$ Important notes Design value of the ultimate bond stress  $f_{bd,fi}$  under fire exposure for concrete classes C12/15 to C50/60, (all drilling methods):

The design value of the bond strength fbd,fi under fire exposure has to be calculated by the following equation:

 $\mathbf{f}_{bd,fi} = \mathbf{k}_{fi}(\boldsymbol{\theta}) \cdot \mathbf{f}_{bd,PIR} \cdot \gamma_c / \gamma_{M,fi}$ 

fbd,fi Design value of the ultimate bond stress in case of fire in N/mm<sup>2</sup>

$$\begin{aligned} k_{fi}(\theta) &= \frac{10151 \cdot \theta^{-1.791}}{f_{bd,PIR} \cdot 4.3} \leq 1.0 \qquad \theta \leq 172^{\circ}C \\ k_{fi}(\theta) &= 0 \qquad \qquad \theta > 172^{\circ}C \end{aligned}$$

θ Temperature in °C in the mortar layer.

 $k_{fi}(\theta)$  Reduction factor under fire exposure.

- f<sub>bd,PIR</sub> Design value of the ultimate bond stress in N/mm<sup>2</sup> in cold condition according to Table C3 considering the concrete classes, the rebar diameter, the drilling method and the bond conditions according to EN 1992-1-1.
- $\gamma_c$  partially safety factor according to EN 1992-1-1

 $\gamma_{M,fi}$  partially safety factor according to EN 1992-1-2

For evidence under fire exposure the anchorage length shall be calculated according to EN 1992-1-1:2004+AC:2010 Equation 8.3 using the temperature-dependent ultimate bond stress  $f_{bd,fi}$ .

# Example graph of Reduction factor $k_{fi}(\theta)$ for concrete classes C20/25 for good bond conditions:

